

APPARATUS AND METHOD FOR PROVIDING CONTAINER INTERIOR
STERILIZATION IN AN ASEPTIC PROCESSING APPARATUS

FIELD OF THE INVENTION

5 The present invention relates generally to systems for
the aseptic packaging of food products. More particularly,
the present invention relates to an apparatus and method for
providing container interior sterilization in an aseptic
processing apparatus.

BACKGROUND OF THE INVENTION

10 Sterilized packaging systems in which a sterile food
product is placed and sealed in a container to preserve the
product for later use are well known in the art. Methods of
sterilizing incoming containers, filling the containers with
pasteurized product, and sealing the containers in an
15 aseptic sterilization tunnel are also known.

Generally, containers such as cups are sterilized using

a mixture of hydrogen peroxide and a carrier gas such as air. The hydrogen peroxide vapor mixture is directed against the interior surface of the cup and a condensate film forms. Cups typically have a ratio of an opening diameter to a height of greater than 1.0. The hydrogen peroxide vapor may be easily introduced through the large opening and the vapor easily covers the interior surface of the cup. Furthermore, a hot drying gas may easily flow through and dry the interior of the cup. For containers such as bottles, with an opening to a height ratio of less than 1.0, difficulties arise in attempting to sterilize to aseptic standards the large interior surface. For example, difficulties occur when trying to rapidly introduce a sterilant through the small bottle opening onto the large interior surface. It is difficult to achieve a uniform coating of sterilant over the interior surface. Additionally, the sterilant vapor may condense and form droplets on the surface. These droplets are difficult to remove and can cause residual sterilant levels above an acceptable level. For example, for the sterilant hydrogen peroxide, the residual level must be less than .5 PPM in

order to meet FDA standards. The small bottle opening also restricts the flow of drying gas that can enter, pass through, and exit the bottle.

Another disadvantage in the design of typical hydrogen peroxide sterilization equipment is the build up of hydrogen peroxide droplets in the delivery nozzles or other delivery apparatus. These droplets can eventually be directed into the container and become impossible to heat and evaporate, and therefore, will result in a residual level of hydrogen peroxide in the container which will be greater than the FDA allowable 0.5 PPM.

Packaged food products can generally be categorized as high acid products (Ph below 4.5) or low acid products (Ph of 4.5 and above). The high acid content of a high acid product helps to reduce bacteria growth in the product, thereby increasing the shelf life of the product. The low acid content of a low acid product, however, necessitates the use of more stringent packaging techniques, and often requires refrigeration of the product at the point of sale.

Several packaging techniques, including extended shelf life (ESL) and aseptic packaging, have been developed to

increase the shelf life of low acid products. During ESL packaging, for example, the packaging material is commonly sanitized and filled with a product in a presterilized tunnel under "ultra-clean" conditions. By using such ESL packaging techniques, the shelf life of an ESL packaged product is commonly extended from about 10 to 15 days to about 90 days. Aseptic packaging techniques, however, which require that the packaging take place in a sterile environment, using presterilized containers, etc., are capable of providing a packaged product having an even longer shelf life of 150 days or more. In fact, with aseptic packaging, the shelf life limitation is often determined by the quality of the taste of the packaged product, rather than by a limitation caused by bacterial growth.

For the aseptic packaging of food products, an aseptic filler must, for example, use an FDA (Food and Drug Administration) approved sterilant, meet FDA quality control standards, use a sterile tunnel or clean room, and must aseptically treat all packaging material. The food product must also be processed using an "Ultra High Temperature"

(UHT) pasteurization process to meet FDA aseptic standards. The packaging material must remain in a sterile environment during filling, closure, and sealing operations.

Many attempts have been made, albeit unsuccessfully, to
5 aseptically fill containers, such as bottles or jars having
small openings, at a high output processing speed. In
addition, previous attempts for aseptically packaging a low
acid product in plastic bottles or jars (e.g., formed of
polyethylene terephthalate (PET) or high density polyethylene
(HDPE)), at a high output processing speed, have also
failed. Furthermore, the other fillers have not been
successful in providing a high output aseptic filler that
complies with the stringent United States FDA standards for
labeling a packaged product as "aseptic." In the following
description of the present invention, the term "aseptic"
denotes the United States FDA level of aseptic.

SUMMARY OF THE INVENTION

In order to overcome the above deficiencies, the
20 present invention provides an apparatus and method for

providing container interior sterilization in an aseptic processing apparatus. The interior container sterilization is applied in an apparatus for providing aseptically processed low acid products in a container having a small opening, such as a glass or plastic bottle or jar, at a high output processing speed. The present invention includes a plurality of sterile air supply sources. For example, a first supply source of sterile air is used to atomize a sterilant (e.g., hydrogen peroxide), within an atomizing venturi. A second supply source of sterile air is used to provide hot sterile air to the atomized sterilant leaving the atomizing venturi. A third supply source of sterile air is used to provide hot sterile air for activating and drying the sterilant on the interior surface of the container. The second supply source of heated sterile air, prevents the formation of hydrogen peroxide droplets. This results in a design that will meet the FDA regulations for each and every bottle that is manufactured. Typically, in the aseptic packaging industry, a low volume of air at a high temperature is applied to the packaging materials. This method works well when the container material can withstand

relatively high temperatures such as when cups are made of polypropylene. However, this often results in deformation and softening of packaging materials formed of PET or HDPE. In order to prevent softening and deformation of the bottles, when formed from these types of plastic materials, the present invention applies high volumes of air at relatively low temperatures over an extended period of time in the activation and drying apparatus. A long exposure time is predicated by the geometry of the bottle and the softening temperature of the material used to form the bottle. In the present invention, about 24 seconds are allowed for directing hot sterile air from the third supply source of sterile air into the interior of the bottles. In order to achieve aseptic sterilization, the bottle is maintained at about 131°F for at least 5 seconds. Many features are incorporated into the interior bottle sterilization apparatus in order to meet the various FDA aseptic standards and the 3A Sanitary Standards and Accepted Practices.

The present invention generally provides an apparatus comprising:

a first supply source of sterile air;

a supply source of sterilant;

5 an atomizing system producing an atomized sterilant from the mixing of the sterile air from the first supply source of sterile air with the sterilant;

a second supply source of a hot sterile air for providing the hot sterile air to the atomized sterilant;

a probe for applying the atomized sterilant into an interior of a container; and

a third supply source of a hot sterile drying air for activating and drying the sterilant in the interior of the container.

Also provided is a method comprising:

providing a first supply of sterile air;

providing a supply of sterilant;

producing an atomized sterilant by mixing the first supply of sterile air with the sterilant;

20 providing a second supply of hot sterile air to the atomized sterilant;

providing a probe for applying the atomized
sterilant into an interior of a container; and

supplying a third supply of hot sterile drying air
for activating and drying the sterilant in the interior of
the container.

BRIEF DESCRIPTION OF THE DRAWINGS

The features of the present invention will best be
understood from a detailed description of the invention and
a preferred embodiment, thereof selected for the purposes of
illustration, and shown in the accompanying drawings in
which:

FIG. 1 is a plan view of an aseptic processing
apparatus in accordance with a preferred embodiment of the
present invention;

FIG. 2 is a side view of the aseptic processing
apparatus of FIG. 1;

FIG. 3 is a partial cross-sectional side view of the
aseptic processing apparatus of FIG. 1;

FIG. 4 is a cross-sectional side view of a bottle
infeed and sterilization apparatus;

FIG. 5 illustrates a cross-sectional top view of the
bottle infeed and sterilization apparatus taken along line
5 5--5 of FIG. 4;

FIG. 6 is an interior sectional view of an interior
wall taken along line 6--6 of FIG. 4;

FIG. 7 is a cross-sectional view of the bottle infeed
and sterilization apparatus taken along line 7--7 of FIG. 4;

FIG. 8 is a perspective view of a conveying plate for
use in the aseptic processing apparatus of the present
invention;

FIG. 9 is a perspective view of a partition in a
sterilization tunnel;

FIG. 10 is a cross-sectional side view of an interior
bottle sterilization apparatus and the partition located
between stations 8 and 9;

FIG. 11 is a cross-sectional side view of the partition
located between stations 22 and 23;

FIG. 12 is a cross-sectional side view of the partition
located between stations 35 and 36;

FIG. 13 is a cross-sectional side view of a lid sterilization and heat sealing apparatus;

FIG. 14 is a side view of a lifting apparatus with a gripper mechanism for lifting the bottles from the sterilization tunnel;

FIG. 15 is a top view of the aseptic processing apparatus;

FIG. 16 is a side view of the aseptic processing apparatus indicating the control and monitoring locations that are interfaced with a control system;

FIG. 17 is a plan view of a daisy chain of lids;

FIG. 18 is a plan view of another embodiment of a daisy chain of lids with holes for receiving pins of a drive wheel;

FIG. 19 is another embodiment of the lid sterilization and heat sealing apparatus including a pin drive apparatus;

FIG. 20 is a perspective view of the heat sealing and gripper apparatus; and

FIG. 21 is a schematic diagram of a sterilization control system for the interior bottle sterilization apparatus.

DETAILED DESCRIPTION OF THE INVENTION

Although certain preferred embodiments of the present invention will be shown and described in detail, it should be understood that various changes and modifications may be made without departing from the scope of the appended claims. The scope of the present invention will in no way be limited to the number of constituting components, the materials thereof, the shapes thereof, the relative arrangement thereof, etc., and are disclosed simply as an example of the preferred embodiment. The features and advantages of the present invention are illustrated in detail in the accompanying drawings, wherein like reference numerals refer to like elements throughout the drawings. Although the drawings are intended to illustrate the present invention, the drawings are not necessarily drawn to scale.

The present invention provides an aseptic processing apparatus 10 that will meet the stringent United States FDA (Food and Drug Administration) requirements and 3A Sanitary

Standards and Accepted Practices required to label a food product (foodstuffs) as "aseptic". Hereafter, "aseptic" will refer to the FDA level of aseptic. The present invention provides an aseptic processing apparatus 10 for producing at least about a 12 log reduction of *Clostridium botulinum* in food products. In addition, the present invention produces packaging material with at least about a 6 log reduction of spores. Actual testing of the aseptic processing apparatus is accomplished with spore test organisms. These test organisms are selected on their resistance to the media selected used to achieve sterility. For example, when steam is the media, the test organism is *Bacillus stearothermophilus*. When hydrogen peroxide is the media, then the test organism is *Bacillus subtilis* var. *globigii*.

The present invention processes containers such as bottles or jars that have a small opening compared to its height and its greatest width (e.g., the ratio of the opening diameter to the height of the container is less than 1.0). In the preferred embodiment, a bottle 12 (see, e.g., FIG. 8) is illustrated as the container. The container may

alternately comprise a jar. The bottle 12 is preferably formed of a plastic such as polyethylene terephthalate (PET) or high density polyethylene (HDPE), although other materials such as glass may also be used. The present invention uses an aseptic sterilant such as hydrogen peroxide (H_2O_2) or oxonia (hydrogen peroxide and peroxyacetic acid) to sterilize the bottles 12. In the preferred embodiment of the present invention, hydrogen peroxide is used as the sterilant. The present invention uses hydrogen peroxide with a concentration of less than about 35% and ensures that the bottles 12 have less than about .5ppm of residual hydrogen peroxide after each bottle 12 is sterilized.

FIGS. 1-3 illustrate several views of an aseptic processing apparatus 10 in accordance with a preferred embodiment of the present invention. As shown, the aseptic processing apparatus 10 includes a first bottle unscrambler 20, a second bottle unscrambler 30, and a bottle lifter 40 for providing a supply of properly oriented empty bottles. The empty bottles are delivered to a filler apparatus 50 after passing through a bottle infeed and sterilization

apparatus 60 for aseptic sterilization. The filled bottles are sealed at a first capping apparatus 400 or a second capping apparatus 410. A control system 550 monitors and controls the operation of the aseptic processing apparatus 10. The filled and sealed bottles are packed and palletized using a first case packing apparatus 480, a second case packing apparatus 490, a first palletizer 500, and a second palletizer 510.

The bottles 12 arrive at a first bottle unscrambler 20 with a random orientation, such that an opening 16 (see FIG. 8) of each bottle 12 can be oriented in any direction. The first bottle unscrambler 20 manipulates the bottles 12 until the opening 16 of each bottle 12 is in a top vertical position. The bottles 12 leave the first bottle unscrambler 20 in a series formation with the opening 16 of each bottle 12 oriented vertically. The bottles 12 travel in single file in a first lane 18 to a first bottle lifter 40. The first bottle lifter 40 lifts and transports the bottles 12 to a bottle infeed and sterilization apparatus 60. A second bottle unscrambler 30 may also be used to provide a supply of vertically oriented bottles 12. The bottles 12 output from

the second bottle unscrambler 30 travel in single file in a second lane 22 to a second bottle lifter 42, which lifts and transports the bottles 12 to the bottle infeed and sterilization apparatus 60.

5 FIG. 3 illustrates the bottle infeed, sterilization, and conveying apparatus 60 attached to the filler apparatus 50. FIG. 4 illustrates a cross-sectional side view of the bottle infeed, sterilization, and conveying apparatus 60. FIG. 5 illustrates a cross-sectional top view of the bottle infeed, sterilization, and conveying apparatus 60 taken along line 5--5 of FIG. 4. The bottle infeed and sterilization apparatus 60 preferably inputs six bottles 12 in a horizontal direction from the first lane 18 and six bottles in a horizontal direction from the second lane 22 (FIG. 5). A gate 76 in the first lane 18 selectively groups six bottles 12 at a time in first horizontal row 24. A gate 78 in the second lane 22 selectively groups six bottles 12 at a time in a second horizontal row 28. An infeed apparatus 80 includes a pushing element 84 for pushing the
20 bottles 12 in the first horizontal row 24 into a first vertical lane 26. A corresponding infeed apparatus 80

includes a pushing element 86 for pushing the bottles 12 in the second horizontal row 28 into a second vertical lane 32. The six bottles 12 in the first vertical lane 26 and the six bottles 12 in the second vertical lane 32 are directed
5 downward into the bottle infeed and sterilization apparatus 60.

Referring to FIG. 4, as the bottles 12 move downward in the first vertical lane 26 and the second vertical lane 32, a sterilant 14, such as heated hydrogen peroxide, oxonia, or other aseptic sterilant, is applied to an outside surface 34 of each bottle 12 by a sterilant application apparatus 36. The outside surface 34 of a bottle 12 is illustrated in greater detail in FIG. 8. The bottles 12 may move downward in the first vertical lane 26 and the second vertical lane 32 by the force of gravity. Alternatively, controlled downward movement of the bottles 12 can be created by the use of a conveying device such as a moving conveying chain. A plurality of pins are attached to the conveying chain. Each bottle 12 rests on one of the pins attached to the
20 conveying chain. Therefore, the motion of each bottle is controlled by the speed of the moving conveying chain.

A sterilant such as hydrogen peroxide may be provided to the sterilant application apparatus 36 in many ways. For example, liquid hydrogen peroxide may be provided in a reservoir at a level maintained by a pump and overflow pipe. A plurality of measuring cups (e.g., approximately 0.5ml each) connected by an air cylinder are submerged into the reservoir and are lifted above the liquid level. Thus, a measured volume of liquid hydrogen peroxide is contained in each measuring cup.

Each measuring cup may include a conductivity probe that is configured to send a signal to the control system 550 indicating that the measuring cup is full. A tube (e.g., having a diameter of about 1/16") is positioned in the center of the measuring cup. A first end of the tube is positioned near the bottom of the measuring cup. A second end of the tube is connected to the sterilant application apparatus 36. The sterilant application apparatus 36 includes a venturi and a heated double tube heat exchanger. When the measuring cup is full, and a signal is received from the control system 550, a valve is opened allowing pressurized sterile air to enter the venturi. The

pressurized air flow causes a vacuum to be generated in
second end of the tube causing liquid hydrogen peroxide to
be pulled out of the measuring cup. The liquid hydrogen
peroxide is sprayed into a sterile air stream which atomizes
the hydrogen peroxide into a spray. The atomized hydrogen
peroxide enters the double tube heat exchanger in order to
heat the atomized hydrogen peroxide above its vaporization
phase. The double tube heat exchanger is heated with steam
and the temperature is monitored and controlled by the
control system 550. In FIG. 4, the application of the
sterilant 14 by the sterilant application apparatus 36 is
accomplished through the use of spray nozzles 64 that
produce a sterilant fog which is directed to the entire
outside surface 34 of each bottle 12.

Alternatively, a direct spray of heated hydrogen
peroxide may be continuously applied to the outside surface
34 of each bottle 12. For producing the direct spray, a
metering pump regulates the amount of hydrogen peroxide, a
flow meter continuously measures and records the quantity of
hydrogen peroxide being dispensed, a spray nozzle produces a
fine mist, and a heat exchanger heats the hydrogen peroxide

above the vaporization point.

FIGS. 3 and 4 illustrate the sterilization chamber 38 for activation and drying of bottles 12 which is included in the bottle infeed, sterilization, and conveying apparatus 60. The sterilization chamber 38 sterilizes the outside surface 34 of each bottle 12. The sterilization chamber 38 encloses a conduit 39. Sterile heated air, which is generated by a sterile air supply system 146 (FIG. 3), enters the conduit 39 of the sterilization chamber 38 through ports 67 and 68 located at the bottom of the sterilization chamber 38. The sterile heated air also enters through a bottom opening 62 of the bottle infeed and sterilization apparatus 60. The sterile heated air travels up through the conduit 39 of the sterilization chamber 38, and exits the top of the sterilization chamber 38 through an exhaust conduit 70. The sterile heated air continuously flows in an upward direction through the sterilization chamber 38, thus preventing any contaminants from entering the bottle infeed and sterilization apparatus 60. To create the sterile heated air, the air is first passed through a filtering system (e.g., a group of double sterile air

filters to sterilize the air. The air is then heated in a heating system (e.g., an electric heater) to about 230°F. The air temperature is regulated by the control system 550. Other techniques for providing the sterile heated air may also be used. The control system 550 monitors the air pressure and flow rate of the sterile heated air to ensure that an adequate flow of the hot sterile air is maintained in the bottle sterilization chamber 38 of the bottle infeed and sterilization apparatus 60.

As illustrated in FIGS. 4, 6, and 7, the sterilization chamber 38 includes two opposing, interior, perforated walls 72A, 72B. The perforated walls 72A and 72B guide the bottles 12 downward in the first vertical lane 26 and the second vertical lane 32, respectively. The perforated walls 72A, 72B also allow the complete circulation of hot sterile air around the outside surface 34 of each bottle 12 in the sterilization chamber 38. The sterilization chamber 38 supplies hot sterile air to the outside surface 34 of each bottle 12 between the sterilant application apparatus 36 and the bottom opening 62 of the bottle infeed and sterilization apparatus 60. This sterilant may be hydrogen peroxide or

oxonia (hydrogen peroxide and peroxyacetic acid).

In accordance with the preferred embodiment of the present invention, twelve drying positions are provided in the sterilization chamber 38. Each bottle 12 is exposed to the hot sterile air in the sterilization chamber 38 for about at least 24 seconds. This provides time sufficient time for the hydrogen peroxide sterilant to break down into water and oxygen, to kill any bacteria on the bottles 12, and to evaporate from the outside surface 34 of the bottles 12.

An exhaust fan 73 is located at a top of the exhaust conduit 70 to provide an outlet from the sterilization tunnel 90, and to control the sterile air flow rate through the sterilization chamber 38. The exhaust fan 73 is controlled by the control system 550. The control system 550 controls the sterile air temperature preferably to about 230°F, and controls the sterile air flow rate through the sterilization chamber 38. The flow rate is preferably about 1800 scfm through the sterilization chamber 38. The bottles 12 leave the sterilization chamber 38 with a hydrogen peroxide concentration of less than 0.5PPM.

As shown in FIGS. 3 and 4, a plurality of proximity sensors 71 located along the sides of the vertical lanes 26, 32 detect any bottle 12 jams that occur within the sterilization chamber 38. The proximity sensors 71 transmit an alarm signal to the control system 550. The bottles 12 leave the bottle infeed and sterilization apparatus 60 through the bottom opening 62, and enter a sterilization tunnel 90 of the filler apparatus 50.

In the preferred embodiment of the present invention, the filler apparatus 50 includes forty-one (41) index stations 92, hereafter referred to as "stations." Various index stations 92 are illustrated in FIGS. 3, 4, and 11-15. The conveying motion of the bottles 12 to the various stations 92 through the filler apparatus 50 is based on an indexing motion. The filler apparatus 50 is designed to convey the bottles 12 through the various operations of the filler 50 in a two by six matrix. The twelve bottles 12 in the two by six matrix are positioned in, and displaced by, a conveying plate 94 as illustrated in FIG. 8. Therefore, twelve bottles 12 are exposed to a particular station 92 at the same time. A conveying apparatus 100 moves the set of

twelve bottles 12 in each conveying plate 94 sequentially through each station 92.

Referring to FIGS. 3 and 4, the bottles 12 are supplied from an infeed chamber 102 to station 2 of the filler apparatus 50 through the bottom opening 62 of the bottle infeed and sterilization apparatus 60. The infeed chamber 102 is enclosed to direct heated hydrogen peroxide laden air completely around the outer surface 34 of the bottles 12. A mechanical scissors mechanism and a vacuum "pick and place" apparatus 104 position twelve bottles 12 at a time (in a two by six matrix, FIG. 8) into one of the conveying plates 94.

A plurality of conveying plates 94 are attached to a main conveyor 106. The main conveyor 106 forms a continuous element around conveyor pulleys 108 and 110 as illustrated in FIG. 3. A bottle support plate 107 supports a bottom 120 of each bottle 12 as the bottles 12 are conveyed from station to station through the filler apparatus 50. Each conveying plate 94 passes through stations 1 through 41, around pulley 108, and returns around pulley 110 to repeat the process. The main conveyor 106, conveying plates 94, and pulleys 108 and 110 are enclosed in the sterilization

tunnel 90.

At station 4, the bottles 12 in the conveying plate 94 enter a bottle detection apparatus 112. The bottle detection apparatus 112 determines whether all twelve bottles 12 are actually present and correctly positioned in the conveying plate 94. Proximity sensors 114 detect the presence and the alignment of each bottle 12. In the present invention, a bottle 12 with correct alignment is in an upright position with the opening 16 of the bottle 12 located in an upward position. Information regarding the location of any misaligned or missing bottles 12 is relayed to the control system 550. The control system 550 uses this location information to ensure that, at future stations 92, bottle filling or sealing will not occur at the locations corresponding to the misaligned or missing bottles 12.

At station 7, as illustrated in FIGS. 3 and 10, the bottles 12 in the conveying plate 94 enter an interior bottle sterilization apparatus 116. A sterilant, such as hydrogen peroxide, oxonia, or any other suitable aseptic sterilant is applied as a heated vapor fog into the interior 118 of each bottle 12. Preferably, hydrogen peroxide is

used as the sterilant in the present invention. The application of sterilant is accomplished with the use of a plurality of sterilant measuring devices 121 and a plurality of probes 123. Each probe 123 includes any practical means for transferring the sterilant from the probe 123 to the interior surface 119 of the bottle 12. For example, an opening or a plurality of openings may be used for ejecting the sterilant onto the interior surface 119. Preferably, in the present invention, an applicator spray nozzle 122 is included in each probe 123. The applicator spray nozzle 122 provides uniform sterilant application without droplet formation on the interior surface 119 of the bottle 12. A separate measuring device 121 and the probe 123 are used for each of the twelve bottle 12 locations in the conveying plate 94. Each sterilant measuring device 121 may include a spoon dipper 304 (e.g., approximately 0.5ml each) as illustrated in FIG. 21. Each bottle 12 is supplied with the same measured quantity of sterilant, preferably in the form of a hot vapor fog. A pump 306 provides a sterilant (e.g., hydrogen peroxide) from a sterilant supply tank 310 to a reservoir 124. An overflow pipe 308 maintains the sterilant

liquid level in the reservoir 124 by returning excess
sterilant to the sterilant supply tank 310. The spoon
dipper 304 connected to an air cylinder 316 is submerged
into the reservoir 124 and is lifted above the liquid level.

5 Thus, a measured volume of liquid hydrogen peroxide (e.g.,
approximately 0.5ml) is contained in each spoon dipper 304.

Each spoon dipper 304 may include a conductivity probe
that is configured to send a signal to the control system
550 indicating that the spoon dipper 304 is full. A tube
312 (e.g., having a diameter of about 1/16") is positioned
in the center of the spoon dipper 304. A first end of the
tube 312 is positioned near the bottom of the spoon dipper
304. A second end of the tube 312 is connected to an
atomizing venturi 314.

A pressurized air source 318 is connected by a conduit
320 to a flow adjust valve 322. A conduit 324 connects the
flow adjust valve 322 to a regulator valve 326. A conduit
328 connects the regulator valve 326 with a solenoid
actuated valve 330. A conduit 332 connects the solenoid
20 actuated valve 330 with the air cylinder 316. The control
system 550 controls the solenoid actuated valve 330 which

controls the compressed air supplied to the air cylinder 316. Compressed air supplied to the air cylinder 316 lowers or lifts the spoon dipper 304 into or out of the liquid sterilant.

5 A conduit 334 connects the flow adjust valve 322 with the regulator valve 336. A conduit 338 connects the regulator valve 336 with a sterile air filter 340. A conduit 342 connects the sterile air filter 340 with a solenoid actuated valve 344. A conduit 346 connects the solenoid actuated valve 344 with the atomizing venturi 314. When the spoon dipper 304 is full, and a signal is received from the control system 550, the solenoid actuated valve 344 is opened allowing pressurized sterile air to enter the atomizing venturi 314 through the conduit 346. The pressurized air flow causes a vacuum to be generated in the second end of the tube 312 causing liquid hydrogen peroxide to be pulled out of the spoon dipper 304.

 A first supply of sterile air is supplied through conduit 346. The pressurized air supplied through conduit 346 is used to atomize the hydrogen peroxide sterilant in the atomizing venturi 314. Atomization of the liquid

continuously supplying humidity controlled air to the heater
368. The flow of heated sterile air is controlled with the
flow adjust valve 376 and travels through conduit 378.

5 Exiting conduit 378, the second supply of hot sterile
air enters the conduit 348 to mix with the atomized hydrogen
peroxide from the atomizing venturi 314. Excess flow of
heated sterile air travels through conduit 380 and passes
through the bypass valve 382. The second supply of hot
sterile air assists in obtaining a uniform concentration of
hydrogen peroxide in the air stream in conduit 348 and
provides enough momentum to ensure that all portions of the
bottle 12 interior 118 are contacted by hydrogen peroxide.
Furthermore, the second supply of hot sterile air is
continuously blowing, whereas the first supply of sterile
air and hydrogen peroxide in conduit 346 is intermittent
corresponding to the movement of the bottles 12. Since the
second supply of hot sterile air is continuous, hydrogen
peroxide does not have the ability to fall out of the air
stream and deposit in the delivery conduit 348 in the form
20 of drops. This ensures that the delivery of hydrogen
peroxide is consistent from one bottle 12 application to the

next and does not allow a drop to be directed into the
bottle 12 interior 118.

5 The mixture of heated sterile air and atomized hydrogen
peroxide in conduit 348 passes through the double tube heat
exchanger 350. The double tube heat exchanger 350 adds
additional heat to the atomized hydrogen peroxide. Heat is
supplied to the double tube heat exchanger 350 from the
steam supply 354 controlled by the regulator valve 360.
Generally, hydrogen peroxide has chemical stabilizers in it
that may cause a white powder precipitate to form on the
inner surfaces of the double tube heat exchanger 350. This
occurs when the temperature differential between the
supplied steam heat and the gas to be heated is large. In
the present invention, the temperature of the atomized
hydrogen peroxide is typically about the same as the
supplied steam heat so that a minimal amount of precipitate
occurs. Another embodiment of the invention eliminates the
need for the double tube heat exchanger 350 because the
temperature of the atomized hydrogen peroxide is already at
20 the desired temperature.

The temperature of the atomized gas entering the interior 118 of the bottle 12 is in the range of about 100°C to 120°C. This temperature is limited to prevent the plastic bottles 12 from melting. The droplet size occurring on the interior surface 119 of the bottles 12 is in the range of about 300 to 500 micrometers. The initial concentration level of hydrogen peroxide on the interior surface 119 of the bottle 12 is about 35%.

As illustrated in FIG. 21, the control system 550 monitors the temperatures at locations denoted as "T" in the interior bottle sterilization apparatus 116. The ~~temperatures~~ ^{temperatures} "T" are measured in the conduit 348, in the heater 368, and in the conduit 370. Additionally, the control system 550 monitors the pressures at locations denoted as "P" as illustrated in FIG. 21. The pressures "P" are measured in the conduit 328, conduit 338, and in the conduit 382.

The control system 550 monitors and controls a spray apparatus 126 that includes the probe 123 including the applicator spray nozzles 122 FIG 10. Each applicator spray nozzle 122 sprays the sterilant into the interior 118 of a

corresponding bottle 12 as a hot vapor fog. The probe 123 including applicator spray nozzles 122 are designed to extend through the bottle openings 16. The probe 123 including applicator spray nozzles 122 descends into the interior 118 and toward the bottom of the bottles 12. This ensures the complete application of sterilant to the entire interior 118 and interior surface 119 of each bottle 12. Alternately, the probe 123 including the applicator spray nozzles 122 may be positioned immediately above the bottle openings 16 prior to the application of sterilant.

FIG. 9 illustrates a perspective view of a partition 130 that provides control of sterile air flow within the sterilization tunnel 90 of the filler apparatus 50. The partition 130 includes a top baffle plate 132, a middle baffle plate 134, and a bottom baffle plate 136. The top baffle plate 132 and the middle baffle plate 134 are provided with cut-outs 133 which correspond to the outer shape of each bottle 12 and to the outer shape of the conveyor plate 94. The cut-outs 133 allow each bottle 12 and each conveyor plate 94 to pass through the partition 130. A space 138 between the middle baffle plate 134 and

the bottom baffle plate 136 allows each empty conveyor plate 94 to pass through the partition 130 as it travels on its return trip from the pulley 108 toward the pulley 110.

As illustrated in FIG. 3, partitions 130A, 130B, and 130C, are located within the sterilization tunnel 90. FIG. 10 illustrates a cross-sectional view of partition 130A including baffle plates 132A, 134A, and 136A. The partition 130A is located between stations 8 and 9. FIG. 11 illustrates a cross-sectional view of partition 130B including baffle plates 132B, 134B, and 136B. The partition 130B is located between stations 22 and 23. FIG. 12 illustrates a cross-sectional view of partition 130C including baffles 132C, 134C, and 136C. The partition 130C is located between stations 35 and 36. As illustrated in FIG. 3, sterile air is introduced through sterile air supply sources (e.g., conduits 140, 142, and 144) into the sterilization tunnel 90. The sterile air conduit 140 is located at station 23 (FIG. 11), the sterile air conduit 142 is located at station 27 (FIG. 3), and the sterile air conduit 144 is located at station 35 (FIG. 12).

The partition 130A separates an activation and drying

apparatus 152 from the interior bottle sterilization
apparatus 116. The partition 130B separates the activation
and drying apparatus 152 from a main product filler
apparatus 160 and a lid sterilization and heat sealing
5 apparatus 162. Thus, a first sterilization zone 164 is
created that includes the activation and drying apparatus
152. Partition 130C separates the main product filler
apparatus 160 and the lid sterilization and heat sealing
apparatus 162 from a bottle discharge apparatus 280. Thus,
partitions 130B and 130C create a second sterilization zone
166 that includes the main product filler apparatus 160 and
the lid sterilization and heat sealing apparatus 162. A
third sterilization zone 172 includes the bottle discharge
apparatus 280. A fourth sterilization zone 165 includes the
interior bottle sterilization apparatus 116. The second
sterilization zone 166 provides a highly sterile area where
the bottles 12 are filled with a product and sealed. The
second sterilization zone 166 is at a higher pressure than
the first sterilization zone 164 and the third sterilization
20 zone 172. Therefore, any gas flow leakage is in the
direction from the second sterilization zone 166 out to the

first sterilization zone 164 and the third sterilization zone 172. The first sterilization zone 164 is at a higher pressure than the fourth sterilization zone 165. Therefore, gas flow is in the direction from the first sterilization zone 164 to the fourth sterilization zone 165.

The partitions 130A, 130B, and 130C create sterilization zones 164, 165, 166, and 172 with different concentration levels of gas laden sterilant (e.g., hydrogen peroxide in air). The highest concentration level of sterilant is in the fourth sterilization zone 165. For example, with the sterilant hydrogen peroxide, the concentration level of hydrogen peroxide is about 1000 ppm (parts per million) in the fourth sterilization zone 165. The hydrogen peroxide sterilant level is about 3 ppm in the first sterilization zone 164. The lowest concentration level of sterilant is in the second sterilization zone 166. In the second sterilization zone 166, the hydrogen peroxide sterilant concentration level is less than .5ppm and typically about .1ppm. Advantageously, this helps to maintain the main product filler apparatus 160 and the lid sterilization and heat sealing apparatus 162 at a low

sterilant concentration level. This prevents unwanted high levels of sterilant to enter the food product during the filling and lidding process. The hydrogen peroxide sterilant concentration level is about .1 ppm in the third sterilization zone 172.

As illustrated in FIG. 3, a gas such as hot sterile air enters the first sterilization zone 164 at a rate of about 2400 cfm (cubic feet per minute). The temperature of the hot sterile air is about 230°F. The hot sterile air enters the first sterilization zone 164 through conduit 148. Additional hot sterile air enters the second sterile zone through sterile air conduits 140, 142, and 144 at a total rate of about 1000 cfm (FIG. 3). Also, hot sterile air enters at a rate of about 1800 cfm through ports 67 and 68 leading into the infeed and sterilization apparatus 60. A portion of the hot sterile air exits the sterilization tunnel 90 at a rate of about 1500 cfm through a plurality of exhaust ports 153 located in the first sterilization zone 164 (FIG. 15). A portion of the hot sterile air exits the sterilization tunnel 90 at a rate about 100 cfm through an opening 282 (FIG. 14). The bottles 12 exit the

sterilization tunnel 90 through the opening 282. The continuous flow of sterile air flow out through the opening 282 prevents contaminants from entering the sterilization tunnel 90.

5 As illustrated in FIG. 3, the hot sterile air is drawn out of the fourth sterilization zone 165 of the sterilization tunnel 90 through the bottom opening 62 in the bottle infeed and sterilization apparatus 60. Next, the hot sterile air from the infeed and sterilization apparatus together with the fourth sterilization zone 165 exits out of the exhaust conduit 70 of the infeed and sterilization apparatus at a rate of about 3600 cfm. This outflow of hot sterile air from the bottle infeed and sterilization apparatus 60 prevents contaminants from entering the bottle infeed sterilization apparatus 60 and the sterilization tunnel 90.

Stations 10 through 21 include twelve stations for directing hot sterile air into each bottle 12 for the activation and removal of the sterilant from the interior of the bottle 12. In these twelve stations, a third supply of hot sterile air is provided through the sterile air supply

system 146. The sterile air supply system 146 supplies hot sterile air to a plurality of nozzles 150 in the activation and drying apparatus 152. The hot sterile air flow in each bottle 12 is about 40 SCFM. Hot sterile air is supplied to the sterile air supply system 146 through conduit 148. The air is first passed through a filtration system to sterilize the air. The air is then heated in a heating system to about 230°F. The air temperature is regulated by the control system 550. Also, the control system 550 monitors the air pressure and flow rate to ensure that an adequate flow of hot sterile air is maintained in the sterilization tunnel 90 of the application and drying apparatus 152.

As shown in FIG. 8, each bottle 12 generally has a small opening 16 compared to its height "H." A ratio of a diameter "D" of the bottle 12 to the height "H" of the bottle 12 is generally less than 1.0. The small bottle opening 16 combined with a larger height "H" restricts the flow of hot gas into the interior 118 of the bottle 12. Also, PET and HDPE bottle materials have low heat resistance temperatures. These temperatures commonly are about 55°C for PET and about 121°C for HDPE. Typically, in the aseptic

packaging industry, a low volume of air at a high temperature is applied to the packaging materials. This often results in deformation and softening of packaging materials formed of PET and HDPE. In order to prevent softening and deformation of the bottles 12, when formed from these types of materials, the present invention applies high volumes of air at relatively low temperatures over an extended period of time in the activation and drying apparatus 152. The plurality of nozzles 150 of the activation and drying apparatus 152 direct hot sterile air into the interior 118 of each bottle 12 (FIG. 11). A long exposure time is predicated by the geometry of the bottle 12 and the softening temperature of the material used to form the bottle 12. In the present invention, about 24 seconds are allowed for directing hot sterile air from the plurality of nozzles 150 into each bottle for the activation and removal of sterilant from the interior surface 119 of the bottle 12. To achieve aseptic sterilization, a minimum bottle temperature of about 131°F should be held for at least 5 seconds. To achieve this bottle temperature and time requirements, including the time required to heat the

bottle, the sterilant is applied for about 1 second and the hot sterile air is introduced for about 24 seconds. The hot sterile air leaves the nozzles 150 at about 230°F and cools to about 131°F when it enters the bottle 12. The hot sterile air is delivered at a high volume so that the bottle 12 is maintained at about 131°F for at least 5 seconds. The about 24 seconds provides adequate time for the bottle 12 to heat up to about 131°F and to maintain this temperature for at least 5 seconds. After bottle 12 has dried, the residual hydrogen peroxide remaining on the bottle 12 surface is less than 0.5 PPM.

A foodstuff product is first sterilized to eliminate bacteria in the product. An "Ultra High Temperature" (UHT) pasteurization process is required to meet the aseptic FDA standard. The time and temperature required to meet the aseptic FDA standard depends on the type of foodstuff. For example, milk must be heated to 282°F for not less than 2 seconds in order to meet the aseptic standards.

After UHT pasteurization, the product is delivered to a main product filler apparatus 160. The main product filler apparatus is illustrated in FIGS. 3 and 13. The main

product filler 160 can be sterilized and cleaned in place to maintain aseptic FDA and 3A standards. A pressurized reservoir apparatus 180 that can be steam sterilized is included in the main product filler apparatus 160. As
5 illustrated in FIG. 13, the pressurized reservoir apparatus 180 includes an enclosed product tank 182 with a large capacity (e.g., 15 gallons). The product tank 182 is able to withstand elevated pressures of about 60 psig or more. The pressurized reservoir apparatus 180 also includes a level sensor 184, a pressure sensor 186, a volumetric measuring device 188, and a filling nozzle 190. The product tank 182 includes a single inlet with a valve cluster including a sterile barrier to separate the product process system from aseptic surge tanks and the main product filler apparatus 160. The product tank 182 has an outlet with twelve connections. At each connections is a volumetric measuring device 188 such as a mass or volumetric flow meter. A plurality of filling nozzles 190A, 190B are provided at stations 23, 25, respectively. In addition,
20 there are a plurality of volumetric measuring devices 188A and 188B to measure the volume of product entering each

bottle 12 at stations 23 and 25, respectively. The control system 550 calculates the desired volume of product to be inserted into each bottle 12, and controls the product volume by opening or closing a plurality of valves 194A and 194B. The activation mechanisms for valves 194A and 194B have a sterile barrier to prevent contamination of the product. The plurality of valves 194A control the volume of product flowing through a corresponding plurality of nozzles 196A into the bottles 12 at station 23. The plurality of valves 194B control the volume of product flowing through a corresponding plurality of nozzles 196B into the bottles 12 at station 25. The control system 550 uses the previously stored information provided by the bottle detection apparatus 112 to only allow filling to occur at the locations where bottles 12 are actually present and correctly aligned.

The initial sterilization process for the pressurized reservoir apparatus 180 includes the step of exposing all of the surfaces of the pressurized reservoir apparatus 180 that come in contact with the product to steam at temperatures above about 250°F for a minimum of about 30 minutes.

Elements such as cups 198A and 198B are used to block off
nozzle outlets 196A and 196B respectively, to allow a build-
up of steam pressure to about 50 psig inside the pressurized
reservoir apparatus 180. Condensate generated as the steam
5 heats the interior surfaces of the pressurized reservoir
apparatus 180 is collected in the cups 198A and 198B. This
condensate is released when the cups 198A and 198B are
removed from the nozzle outlets 196A and 196B. Once the
interior surfaces of the pressurized reservoir apparatus 180
are sterilized, the steam is shut off, and sterile air is
used to replace the steam. The sterile air reduces the
interior temperature of the pressurized reservoir apparatus
180 to the temperature of the product before the product is
allowed to enter the enclosed product tank 182. Sterile air
is directed through sterile air conduits 142 and 144 into
the second sterilization zone 166 at a volume rate of about
800 scfm (FIG. 13). The sterile air flow entering the
second sterilization zone 166 provides sterile air to the
main product filler apparatus 160 and to the lid
20 sterilization and heat sealing apparatus 162.

The main product filler apparatus 160 includes a

separate filling position for each bottle. The bottle 12
filling operation is completed for six bottles at station 23
and for six bottles at station 25.

FIGS. 3 and 13 illustrate the lid sterilization and
heat sealing apparatus 162. A lid 200 is applied to each of
the twelve bottles 12 at station 31. For a fully aseptic
bottle filler, complete lid 200 sterilization is necessary,
and therefore a sterilant such as hydrogen peroxide is
typically used. In the present invention, the lids are
formed of a material such as foil or plastic. The lids 200
are joined together by a small interconnecting band 203 that
holds them together to form a long continuous chain of lids
200, hereinafter referred to as a "daisy chain" 202. The
daisy chain 202 of lids is illustrated in FIGS. 17. A daisy
chain 202 of lids 200 is placed on each of a plurality of
reels 210. For the twelve bottle configuration of the
present invention, six of the reels 210, each holding a
daisy chain 202 of lids 200, are located on each side of a
heat sealing apparatus 214. Each daisy chain 202 of lids
200 winds off of a corresponding reel 210 and is sterilized,
preferably using a hydrogen peroxide bath 204. The

concentration of hydrogen peroxide can range from about 30 to 40%, however, preferably the concentration is about 35%. Each lid 200 remains in the hydrogen peroxide bath 204 for at least 18 seconds. A plurality of hot sterile air knives 208, which are formed by jets of hot sterile air, activate the hydrogen peroxide to sterilize the lids 200 on the daisy chain 202. The hot sterile air temperature is about 135°C. The hot air knives 208 also remove excess hydrogen peroxide from the lids 200. A plurality of heated platens 205 further dry the lids 200 so that the residual concentration of hydrogen peroxide is less than .5 PPM. The hydrogen peroxide bath 204 prevents any contaminants from entering the sterilization tunnel 90 via the lidding operation.

Once sterilized, the lids 200 enter the sterilization tunnel 90 where they are separated from the daisy chain 202 and placed on a bottle 12. Each lid is slightly larger in diameter than that of the opening 16 of a bottle 12. During the placement of the lid 200 on the bottle 12, a slight mechanical crimp of the lid 200 is formed to locate and hold the lid 200 on the bottle 12. The crimp holds the lid 200 in place on the bottle 12 until the bottle 12 reaches a

station 33 for sealing.

Another embodiment of a lid sterilization and heat sealing apparatus 552 is illustrated in FIG. 19. As illustrated in FIG. 18, the daisy chain 215 of lids 200 includes a hole 207 located in each interconnecting band 203. Each hole 207 receives a pin 209 of a drive sprocket 211.

The daisy chain 215A, 215B of lids 200 is placed on each of a plurality of reels 210 (e.g. 210A and 210B). For the twelve bottle configuration of the present invention, six of the reels 210, each holding a daisy chain 215A, 215B of lids 200, are located on each side of a heat sealing apparatus 214. Each daisy chain 215A, 215B of lids 200 winds off of a corresponding reel 210 and is sterilized preferably using a hydrogen peroxide bath 204. The concentration of hydrogen peroxide can range from about 30 to 40%, however, preferably the concentration is about 35%. The lids 200 remain in the hydrogen peroxide bath 204 for at least 18 seconds. A plurality of hot sterile air knives 208, which are formed by jets of hot sterile air, activate the hydrogen peroxide to sterilize the lids 200 on the daisy

chain 215A, 215B. The hot sterile air temperature is about 135°C. The hot air knives 208 also remove excess hydrogen peroxide from the lids 200. A plurality of heated platens 205 further dry the lids 200 so that the residual

5 concentration of hydrogen peroxide is less than .5 PPM. The hydrogen peroxide bath 204 prevents any contaminants from entering the sterilization tunnel 90 via the lidding operation. The drive sprocket 211A includes a plurality of pins 209 that engage with the holes 207 of the daisy chain 215A. The drive sprocket 211A rotates in a counterclockwise direction and indexes and directs the daisy chain 215A, through a plurality of guides 217A. The guides 217A may include a plurality of rollers 221A to further guide and direct an end 219A of the daisy chain 215A over the bottle 12A. The drive sprocket 211B includes a plurality of pins 209 that engage with the holes 207 of the daisy chain 215B. The drive sprocket 211B rotates in a clockwise direction and indexes and directs the daisy chain 215B through a plurality of guides 217B. The guides 217B may include a plurality of
20 rollers 221B to further guide and direct an end 219B of the daisy chain 215B over the bottle 12B.

Once sterilized, the lids 200 enter the sterilization tunnel 90 where they are separated from the daisy chain 215A, 217B and placed on the bottle 12A, 12B. At station 33, the lids 200 are applied to the bottles 12. As illustrated in FIGS. 13 and 20, the heat sealing apparatus 214 includes a heated platen 216 that applies heat and pressure against each lid 200 for a predetermined length of time, to form a seal between the lid 200 and the bottle 12A, 12B. Although lidding for a bottle has been described, it should be appreciated that lidding of other containers (e.g. jars) can be provided by the present invention. FIG. 20 illustrates a perspective view of the heat sealing apparatus 214, the daisy chain 215A, the gripper apparatus 554, the bottle 12A, and the conveying plate 94. The lid 200 is located above the bottle opening 16. The gripper apparatus 554 includes a grip 223 for capturing the bottle 12A by a bottle lip 225. The gripper apparatus 554 lifts the bottle 12A in an upward direction so that the lid 200 is pressed between a bottle top lip 227 and the heated platen 216. The interconnecting band 203 severs and separates the lid 200 on the bottle 12 from the next lid on the daisy chain 215A.

The heated platen 216 is in a two by six configuration to seal twelve of the bottles 12 at a time. There is a separate gripper apparatus 554 for each of the twelve bottles 12. After each bottle 12 is sealed, its gripper apparatus 554 lowers and releases the bottle 12 and each bottle 12 continues to station 37.

At station 37, the lid 200 seal and bottle 12 integrity are checked in a known manner by a seal integrity apparatus (not shown) comprising, for example, a bottle squeezing mechanism and a proximity sensor. Each bottle 12 is squeezed by the bottle squeezing mechanism which causes the lid 200 on the bottle 12 to extend upward. The proximity sensor detects if the lid 200 has extended upward, which indicates an acceptable seal, or whether the seal remains flat, which indicates a leaking seal or bottle 12. The location of the defective bottles 12 are recorded by the control system 550 so that the defective bottles will not be packed.

Bottle discharge from the sterilization tunnel 90 of the filler apparatus 50 occurs at stations 38 and 40 as illustrated in FIGS. 3, 13 and 14. A bottle discharge

apparatus 280 is located at stations 38 and 40. At this point in the filler apparatus 50, the filled and sealed bottles 12 are forced in an upward direction such that a top portion 284 of each bottle 12 protrudes through the opening 282 in the sterilization tunnel 90 (FIG. 14). A rotating cam 290 or other suitable means (e.g., an inflatable diaphragm, etc.) may be used to apply a force against the bottom 120 of each bottle 12 to force the bottle 12 in an upward direction.

As illustrated in FIG. 14, the bottle discharge apparatus 280 comprises a lifting apparatus 286 that includes a gripper 288 that grasps the top portion 284 of each bottle 12 and lifts the bottle 12 out through the opening 282 in the sterilization tunnel 90. In order to ensure that contaminated air cannot enter the sterilization tunnel 90, the sterile air in the sterilization tunnel 90 is maintained at a higher pressure than the air outside the sterilization tunnel 90. Thus, sterile air is always flowing out of the sterilization tunnel 90 through the opening 282. In addition, the gripper 288 never enters the sterilization tunnel 90, because the top portion 284 of the

bottle 12 is first lifted out of the sterilization tunnel 90 by the action of the rotating cam 290 before being grabbed by the gripper 288.

FIG. 15 illustrates a top view of the filler apparatus 50 including the bottle infeed and sterilization apparatus 60, the interior bottle sterilization apparatus 116, and the activation and drying apparatus 152. FIG. 15 additionally illustrates the main filler apparatus 160, the lid sterilization and heat sealing apparatus 162, and the bottle discharge apparatus 280.

Referring again to FIGS. 1 and 14, the lifting apparatus 286 lifts the bottles 12 at station 38 and places the bottles 12 in a first lane 292 that transports the bottles 12 to a first capping apparatus 410. In addition, the lifting apparatus 286 lifts the bottles 12 at station 40 and places the bottles 12 in a second lane 294 that transports the bottles 12 to a second capping apparatus 400.

The first capping apparatus 410 secures a cap (not shown) on the top of each bottle 12 in the first lane 292. The second capping apparatus 400 secures a cap on the top of each bottle 12 in the second lane 294. The caps are secured

to the bottles 12 in a manner known in the art. It should be noted that the capping process may be performed outside of the sterilization tunnel 90 because each of the bottles 12 have previously been sealed within the sterilization
5 tunnel 90 by the lid sterilization and heat sealing apparatus 162 using a sterile lid 200.

After capping, the bottles 12 are transported via the first and second lanes 292, 294 to labelers 460 and 470. The first labeling apparatus 470 applies a label to each bottle 12 in the first lane 292. The second labeling apparatus 460 applies a label to each bottle 12 in the second lane 294.

From the first labeling apparatus 470, the bottles 12 are transported along a first set of multiple lanes (e.g., 4) to a first case packing apparatus 490. From the second labeling apparatus 460, the bottles 12 are transported along a second set of multiple lanes to a second case packing apparatus 480. Each case packing apparatus 480, 490 gathers and packs a plurality of the bottles 12 (e.g., twelve) in
20 each case in a suitable (e.g., three by four) matrix.

A first conveyor 296 transports the cases output by

the first case packer 490 to a first palletizer 510. A second conveyor 298 transports the cases output by the second case packer 480 to a second palletizer 500. A vehicle, such as a fork lift truck, then transports the pallets loaded with the cases of bottles 12 to a storage warehouse.

Referring again to FIG. 3, the main conveyor 106 and each conveying plate 94 are cleaned and sanitized once during each revolution of the main conveyor 106. Specifically, after each empty conveying plate 94 passes around the pulley 108, the conveying plate 94 is passed through a liquid sanitizing apparatus 300 and a drying apparatus 302. The liquid sanitizing apparatus 300 sprays a mixture of a sterilizing agent (e.g., oxonia, (hydrogen peroxide and peroxyacetic acid)) over the entire surface of each conveying plate 94 and associated components of the main conveyor 106. In the drying apparatus 302, heated air with is used to dry the main conveyor 106 and conveying plates 94.

Stations 1 through 40 are enclosed in the sterilization tunnel 90. The sterilization tunnel 90 is supplied with air

that is pressurized and sterilized. The interior of the sterilization tunnel 90 is maintained at a pressure higher than the outside environment in order to eliminate contamination during the bottle processing. In addition, to
5 further ensure a sterile environment within the sterilization tunnel 90, the sterile air supply provides a predetermined number of air changes (e.g., 2.5 changes of air per minute) in the sterilization tunnel 90.

Before bottle production is initiated, the bottle infeed and sterilization apparatus 60 and the filler apparatus 50 are preferably sterilized with an aseptic sterilant. For example, a sterilant such as a hot hydrogen peroxide mist may be applied to all interior surfaces of the bottle infeed and sterilization apparatus 60 and the filler apparatus 50. Then, hot sterile air is supplied to activate and remove the hydrogen peroxide, and to dry the interior surfaces of the bottle infeed and sterilization apparatus 60 and the filler apparatus 50.

FIG. 16 is a side view of the aseptic processing apparatus 10 of the present invention indicating the
20 location of the control and monitoring devices that are

interfaced with the control system 550. The control system 550 gathers information and controls process functions in the aseptic processing apparatus 10. A preferred arrangement of the control and monitoring devices are indicated by encircled letters in FIG. 16. A functional description of each of the control and monitoring devices is listed below. It should be noted that these control and monitoring devices are only representative of the types of devices that may be used in the aseptic processing apparatus 10 of the present invention. Other types and combinations of control and monitoring devices may be used without departing from the intended scope of the present invention. Further, control system 550 may respond in different ways to the outputs of the control and monitoring devices. For example, the control system 550 may automatically adjust the operational parameters of the various components of the aseptic processing apparatus 10, may generate and/or log error messages, or may even shut down the entire aseptic processing apparatus 10. In the preferred embodiment of the present invention, the control and monitoring devices include:

- A. A bottle counter to ensure that a predetermined

number of the bottles 12 (e.g., six bottles) on each upper horizontal row 24, 28 enter the loading area of the bottle infeed and sterilization apparatus 60.

B. A proximity sensor to ensure that the first group of bottles 12 has dropped into the first bottle position in the bottle infeed and sterilization apparatus 60.

C1. A conductivity sensor to ensure that the measuring cup used by the sterilant application apparatus 36 is full.

C2. A conductivity sensor to ensure that the measuring cup used by the sterilant application apparatus 36 is emptied in a predetermined time.

C3. A pressure sensor to ensure that the pressure of the air used by the sterilant application apparatus 36 is within predetermined atomization requirements.

C4. A temperature sensor to ensure that each heat heating element used by the sterilant application apparatus 36 is heated to the correct temperature.

D. A proximity sensor (e.g., proximity sensor 71, FIG. 3) to ensure that a bottle jam has not occurred within the bottle infeed and sterilization apparatus 60.

E. A temperature sensor to ensure that the

temperature of the heated sterile air entering the bottle
infeed and sterilization apparatus 60 is correct.

F. A proximity sensor that to ensure that each
conveying plate 94 is fully loaded with bottles 12.

5 G1. A conductivity sensor to ensure that the measuring
cup used by the interior bottle sterilization apparatus 116
is full.

G2. A conductivity sensor to ensure that the measuring
cup used by the interior bottle sterilization apparatus 116
is emptied in a predetermined time.

G3. A pressure sensor to ensure that the pressure of
the air used by the interior bottle sterilization apparatus
116 is within predetermined atomization requirements.

G4. A temperature sensor to ensure that each heat
heating element used by the interior bottle sterilization
apparatus 116 is heated to the correct temperature.

H. A temperature sensor to ensure that the air drying
temperature within the activation and drying apparatus 152
is correct.

20 I. A plurality of flow sensors to ensure that the
airflow rate of the sterile air entering the sterilization

tunnel 90 is correct.

J. A pressure sensor to ensure that the pressure of the sterile air entering the activation and drying apparatus 152 is correct.

5 K. A measuring device (e.g., volumetric measuring device 188, FIG. 3) to ensure that each bottle 12 is filled to a predetermined level.

L. A pressure sensor to ensure that the pressure in the product tank 182 is above a predetermined level.

M. A level sensor to ensure that the level of product in the product tank 182 is maintained at a predetermined level.

N. Proximity sensors to ensure that the daisy chains 202 of lids 200 are present in the lid sterilization and heat sealing apparatus 162

O. A level sensor to ensure that the hydrogen peroxide level in the hydrogen peroxide bath 204 in the lid sterilization and heat sealing apparatus 162 is above a predetermined level.

20 P. A temperature sensor to ensure that the temperature of the hot sterile air knives 208 of the lid

sterilization and heat sealing apparatus 162 is correct.

Q. A temperature sensor to ensure that the heat sealing apparatus 214 is operating at the correct temperature.

5 R. Proximity sensors to ensure that the bottles 12 are discharged from the filler.

S. A speed sensor to measure the speed of the conveying apparatus 100.

T. A concentration sensor to ensure that the concentration of oxonia is maintained at a predetermined level in the sanitizing apparatus 300.

U. A pressure sensor to ensure that the pressure of the oxonia is maintained above a predetermined level in the sanitizing apparatus 300.

V. A temperature sensor to ensure that the drying temperature of the drying apparatus 302 is correct.

The following steps are performed during the "Clean In Place" (CIP) process in the filler apparatus 50;

23. Conductivity sensor to verify caustic and acid concentrations.

24. Temperature sensor to verify "Clean In Place"
solution temperatures.

25. Flow meter to verify "Clean In Place" flow rates.

26. Time is monitored to ensure that adequate cleaning
time is maintained.

The follow steps are performed during sterilization of
the bottle filler apparatus 50;

27. Temperature sensors for measuring steam
temperatures.

28. Proximity sensors to ensure filler nozzle
cleaning/sterilization cups are in position.

29. Temperature sensors for air heating and cooling.

30. Flow meter for hydrogen peroxide injection.

31. Time is monitored to ensure the minimum time
periods are met (steam, hydrogen peroxide application and
activation/drying).

The foregoing description of the present invention has
been presented for purposes of illustration and description.
It is not intended to be exhaustive or to limit the
invention to the precise form disclosed, and many
modifications and variations are possible in light of the

above teaching. Such modifications and variations that may be apparent to a person skilled in the art are intended to be included within the scope of this invention.

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